FRACTIONAL FACTORIAL DESIGN FOR ENERGY SYSTEMS

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Abstra
t

Nowadays, when powerful omputers are one every mans desk, it has be
ome more and more ommon to use omplex energy system models in order to predict the use of electricity and heat in buildings. At the same time it has been harder to grasp the overall solution because of all the details implemented in such a model. A method which could help the operator to find the important parts in the model would therefore be of great interest. Traditionally this is addressed by using so called sensitivity analyses. The most common method is then to change one input parameter a ertain amount and study how mu
h the output is influenced by this change. If the output varies heavily the parameter is supposed to be of more interest than if there is a only small hange. If there is a omplex model, several hundreds of parameters may have to be hanged this way whi
h is very tedious. By the use of modern statistics these calculations can be made in a more planned way and the necessary work be minimized. One such method is fractional factorial design which is used for examining a widely spread Swedish energy balance program with about seventy input data values. We have examined nine of these parameters in order to rank their importan
e for the output energy balan
e. The intera
tion between these nine parameters have also been studied using the same method.

1 INTRODUCTION

In Sweden it is mandatory to show the authorities that the need for heat in a new building is lower or equal to that of a referen
e building presented in the building code. One means for showing this, is to use an energy balance program. The program used by us, where the building is presented in the form of about seventy different values is called ENORM, see Reference [1], which is widely spread in Sweden. The program calculates the energy need and heating demand for a building on a diurnal basis but the result is presented for one year. The program also in
ludes values for the referen
e building and as long as the energy need and demand are lower than that for the referen
e it is allowed to use your own building methods as far as energy onservation is on
erned. Fa
torial design, and fractional factorial design, are statistic methods usually used for bringing down the need for experiments when you must show a scientifically significant output from e.g. a chemical process. The length of this paper does not make

it possible to explain all the details and therefore the in-depth knowledge must be fetched elsewhere, e. g. in Reference $[2]$ chapters $10 - 12$. An example of ordinary fa
torial design for energy systems is re
ently published in Referen
e [3]. However, here we will show a case study where a building is analysed using the ENORM program and the method with fractional factorial design.

CASE STUDY

Factorial design is a method for finding out what an importance a production factor, or in our case a parameter for a building, has on the output result. First you hoose two levels for the parameters of interest, one low level and one high. These levels are shown with "-" and "+" -signs respectively in a so called design matrix. The nine parameters we thought were of major interest, before this work was utilized, are shown in Table 1.

Parameter	Low level	Middle level	High level	Unit
U value, attic joists plus	0.1	0.2	0.3	$\mathrm{W/m^2,K}$
U-value, external wall	0.18	0.35	0.5	$W/m^2, K$
Indoor temperature	18.0	20.0	23.0	\circ \cap
Location, (outdoor temp.)	Malmö	Jönköping	Stockholm	
Building size(area/volume)	135/324	150/360	170/408	$\rm m^2/m^3$
Air renewal rate	0.5	0.5	1.0	1/hour
Heat from appliances	10	12.5	15	kWh/day
Heat recovery system	Exhaust air heat pump Heat exchanger Heat exchanger			
Air tightness		2	3	
Heat loss from air duct no 1	0.04	0.04	0.1	W/m, K
plus air duct no 2	0.2	0.15	0.30	W/m , K

Table 1: The studied parameters

Note that the change in U-values is considered as only one factor due to the way ENORM works. The same is valid for the air duct heat losses. (In the table there is also a middle level whi
h is used later in this paper).

It is not possible, in a paper of this length, to describe all the parameters used for the building. Instead, we only say that the building is a representative for modern low energy buildings ommon in Sweden today. This is shown by the fa
t that if all the low values above are used the total energy need for one year is about 11,000 kWh, while an average of the total building sto
k is about twi
e this value.

If ordinary factorial design was used for the nine parameters above, 2^9 , i. e. 512, different runs of the energy balance program must be made, see Reference [2], page 306. This is a very tedious task but by the use of the fractional method, this number can be significantly reduced. The idea with using only a fraction of the needed experiments emanates from the fact that interaction between the variables tends to get smaller and smaller when the number of intera
ting variables in
reases. (Compare this fa
t with a Taylor series expansion, where terms of the third, and higher, order mostly are neglected). The first thing now is to elaborate the so called design matrix, see Table 2.

This table shows how the experiments, i e. ENORM runs, are to be elaborated in order to achieve as much as possible in terms of statistic result.

The top left mark in the matrix shows us the level of variable number 1, i. e. the U-value for the attic joists. Here, this is a \cdot - \cdot -sign and subsequently the U-

	Setup of levels														
Run number	1	$\overline{2}$	3	$\overline{4}$	1×2	1×3	1×4	2×3	$\overline{2\times 4}$	3×4	5	6	7	8	9
					$+$	$+$	$^{+}$	$^{+}$	$^{+}$	$^+$					
$\overline{2}$	$^+$						\blacksquare	$+$	$+$	$^{+}$	$\hspace{0.1mm} +$	$^+$	$^+$		
3						$^+$	$^+$	\blacksquare		$+$	$+$	$+$	۰		
4	$+$	$^{+}$		-	$\overline{+}$		\blacksquare	\blacksquare		$+$			$^{+}$	\pm	$^+$
5			$^+$	-	$+$		$\, +$	\blacksquare	$^{+}$	۰	$+$	۰	$+$	$^{+}$	
6	$+$	÷	$^+$	\blacksquare		$^+$		\blacksquare	$^{+}$			$\, +$	-	$^+$	$^+$
7		$^+$	\pm	\blacksquare	-		\pm	$+$				$^{+}$	$^+$	÷	$^+$
8	$+$	$+$	$^{+}$	\blacksquare	$^{+}$	\pm	\blacksquare	$^{+}$			$^+$				
9				$\hspace{0.1mm} +$	$+$	$^{+}$	\blacksquare	$+$				$+$	$^+$	$^{+}$	
10	$\, +$			$^{+}$			\pm	$+$			$^{+}$		۰	$^+$	$^+$
11				$+$	-	$^+$		\blacksquare	$^+$		$^{+}$		$^+$	÷	$^+$
12	$^{+}$	$+$	\blacksquare	$+$	$+$		$^+$	\blacksquare	$^{+}$			$^+$			
13			$+$	$+$	$+$					$^{+}$	$+$	$^{+}$			
14	$^{+}$	\blacksquare	$^{+}$	$+$	۰	$^{+}$	$^+$			$+$			$^+$		
15		$^+$	\pm	$\hspace{0.1mm} +$	\blacksquare		\blacksquare	$^+$	$\, +$	$+$					
16	$^+$	$^+$	$^+$	$^{+}$	$^{+}$	$^+$	\pm	$\hspace{0.1mm} +$	$^+$		\pm	$^{+}$	$^+$	$^{+}$	$^+$

Table 2: Design matrix for a 29-5 fractional factorial design

value must equal 0.1 W/m²K in the first energy balance calculation, see Table 1. The second mark is also a "-" -sign and this will likewise lead to the low level for parameter number 2, i. e. the U-value for the external wall, and so on up to column number 4. If we were going to elaborate an ordinary factorial design for four variables the column number 5 would depict the combination of levels for the number 1 and two columns, i.e. multiply the two signs which will result in a $"$ +" -sign. This row is later used for finding out if there is a combination effect between the number 1 and number 2 parameters. Still assuming we are only calculating for four variables, the column that follows the one marked with 3×4 , would show the combination of the levels for parameters 1, 2 and 3. Multiplying these levels results in a "-" -sign. However, these combinations of three or more levels were to be neglected in the fractional version of the method. Instead we insert the parameter number 5, i. e. the air renewal rate in that position. The important thing is that we still must use the low level here be
ause of the calculated "-" -sign. The method will thus result in a "+" -sign for the ninth parameter be
ause this olumn would have been the result of multiplying the four first levels, which all have $"$ -" - signs. Our first experiment must therefore be elaborated by using ENORM with low levels for all parameters, ex
ept for the last one, i. e. heat loss from the ventilation ducts. In order to deal with all the combinations for four parameters we need 24 experiments, i. e. 16 different runs. We have also negle
ted the ombinations for more than two parameters and thus 5 different possibilities are withdrawn. The procedure is therefore called a 29-5 fractional factorial design because we have nine parameters with two levels while five possibilities are neglected, see Reference [2] page 378 and the following, for all details.

In Table 3 the need for energy is shown for all the 16 different ENORM experiments.

In experiment number 1 all parameters but one were at their low level resulting in a need for 11,127 kWh for one year. In experiment number 2 resulting in 22,323 kWh, parameters number 1, 5, 6 and 7 were high while the other were low according to Table 2.

Now the so called main and interaction effects are to be calculated. This is fulfilled by using both Table 2 and 3. According to Reference $[2]$ page 309, these

Run number	Result (kWh/year)
1	11 127
$\overline{2}$	22 323
3	19 246
$\overline{4}$	24 343
5	22 819
6	24 172
7	20 703
8	29 175
9	18 560
10	25 856
11	21 641
12	19416
13	25 970
14	27 363
15	19616
16	38 935

Table 3: The calculated need for purchased electricity in the building, setting the 9 parameters according to the design matrix in Table 2

effects are the same as the difference between the mean average for the values in Table 3 as long as the signs in Table 2 are taken into proper account. The first value in Table 3 is 11,127. For parameter number 1, in Table 2, this value should be considered as negative because there is a "-" -sign in the top left position. For the same parameter the next negative values are found at row number 3, 5, 7 etc. in Table 2. Thus we add all the "positive" values calculate the average, add all the "negative" values, calculate their average and then subtract these values. The pro
edure is shown in detail in the following expression:

$$
\frac{22,323+24,343+24,172+29,175+25,856+19,416+27,363+38,935}{8} - \\ \frac{11,127+19,256+22,819+20,703+18,560+21,641+25,970+19,616}{8} = \\ = 51,901
$$

The other effects are shown in Table 4.

The problem is now to find out which of the effects that are important. When dealing with ordinary experiments this may be found out by omparing the effects to the one found for a normal distribution, i. e. a totally random result. If the same method is used here we must examine if some of the effects in Table 4 are clearly outside of this random behavior. The mean average for the values in Table 4 equals 23,204 while the standard deviation is 5,794. Assuming that the values four standard deviations apart from the average are of interest, we can identify the factors 1, 3, 7 and 9, which are the U-values for the external wall and attic joists, the outdoor temperature, interaction between the U-values and the size of the building, and interaction between the indoor temperature and the size of the house, see Tables 1 and 2.

Factor	Effect	Factor	Effect
1	51,901	9	$-11,167$
$\overline{2}$	14,885	10	6,581
3	46,241	11	40,665
4	23,449	12	7,385
5	9,425	13	22,109
6	9,173	14	15,829
7	-335	15	14,229
x	1,325		

Table 4: Effects for the fractional factorial design

It is somewhat strange that the indoor temperature do not influence on the result more than is found in Table 4 even if there is a strong intera
tion between the indoor temperature and the building size, se factor 9 in Table 4. Sometimes, effects from those parameters which are included as "extras", i. e. number 5 to 9, see Table 2, are overwhelmed by the others. In order to solve this we have elaborated an ordinary factorial design with only those parameters found important above, i. e. the U-values, the indoor temperature, the outdoor temperature and the size of the building, see Ref. $[3]$ for a detailed factorial design dealing with an energy model. This time we have only four parameters to examine and subsequently it is possible to use the same design matrix as shown in Table 1. We only need to change the heading line figures: 5 will now become $1\times2\times3$, 6 will become $1\times2\times4$, 7 will become $1\times3\times4$, 8 will be $2\times3\times4$, while the fifteenth column will represent the interaction between all the four factors, i. e. $1 \times 2 \times 3 \times 4$. All but these four parameters are set to the middle level. In Table 5 the resulting energy need and the calculated main and interaction effects are presented from the sixteen new runs of ENORM.

The average of these effects equals 12,267 while the standard deviation is 17,256. If the same riterion as before, i.e. four standard deviations, is used to depict the factors of interest, none stands out. The same is valid for three intervals, while two standard deviations selects factor number 2 and almost number 1, i. e. indoor temperature and U-values. From Table 5 it is also obvious that intera
tion between the fa
tors is not of high importan
e, the values dwell within plus/minus one standard deviation.

From these two factorial designs it is obvious that the U-value for the building envelope and the temperature difference between the in- and outdoor temperatures are most important for the energy balan
e of a building. Both the fractional and the ordinary factorial design shows this. In the fractional design it was possible to include five extra parameters which, however, were not investigated to the same extent because of the tedious calculation effort needed for this. Further, the fractional factorial design revealed that also the ventilation air renewal rate probably had a big importance, but this effect could be the result from interaction from other parameters.

Run number	Result (kWh/year)	Factor	E ffect
1	16,695	1	43,382
2	20,438	2	54,780
3	21,455	3	14,996
4	27,546	4	19,980
5	17,998	5	10,348
6	21,858	6	598
7	23,476	7	3,476
8	29,735	8	3,188
9	18,216	9	4,334
10	22,607	10	1,100
11	23,792	11	100
12	30,959	12	854
13	19,733	13	28
14	24,256	14	214
15	26,135	15	-2
16	33,483		

Table 5: Result from 16 ENORM runs for different levels of two envelope and two temperature parameters and their main and interaction effects

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h for funding this resear
h.

CONCLUSIONS

The paper shows that it is possible to use statistic methods, such as factorial design, in order to reveal the magnitude of importance of different input data in computer simulation models. By use of factorial design the so called main and interaction effects can be calculated which are measures of their individual and combined influence of the output from a computer program. However, using a lot of input data in the models, even fa
torial design is a very tedious process. Fortunately, this drawback may, at least to some extent, be overcome by use of the fractional method where the interactions between three or more levels are negle
ted. By using these methods for an energy balan
e program for buildings we were able to show that the U-value for the building envelope had the highest importance followed by the difference between the in- and outdoor temperatures. There is also an indication that the ventilation air renewal rate had some major importance for the resulting energy need for the building. For the rest of the studied parameters, for example the type of heat recovery unit, the analysis showed that they had minor importan
e, or that the result was hard to investigate with an ascertained conclusion.

Referen
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